



Edge diffraction in room acoustics computer modelling

U. Peter Svensson¹, Paul T. Calamia²

¹Acoustics Research Centre, Dept. Of Electronics and
Telecommunications, Norwegian University of Science and Technology
(NTNU), Trondheim, Norway

²Program in Architectural Acoustics, School of Architecture,
Rensselaer Polytechnic Institute, Troy, NY, USA

This presentation

Motivation for edge diffraction in room acoustics computer modelling

Three challenges to diffraction modelling

Focus of this paper: how to prune the less important diffraction contributions

Conclusions

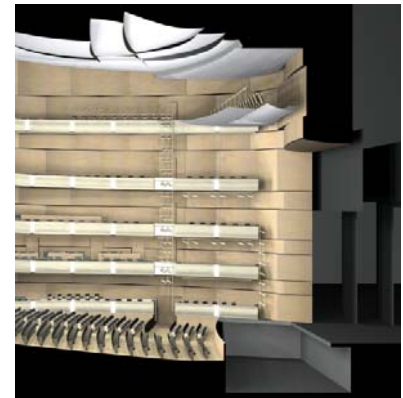
Motivation for edge diffraction modeling in room acoustics

Edge diffraction corrects the discontinuity of specular reflections and gives continuous sound fields.

Examples where diffraction is significant:

1. Reflectors
2. Around corners (orchestra pits, balcony edges,...)
3. Reflections from arches, domes
4. Propagation around pillars

.... but also in any interior space, at low frequencies.



Motivation for edge diffraction modeling in room acoustics

QuickTime™ and a
H.264 decompressor
are needed to see this picture.

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Challenges to edge diffraction modelling

1. Rapid growth of number of components

Main topic of this presentation. How can we find which components could be skipped/pruned?

2. Non-rigid surfaces

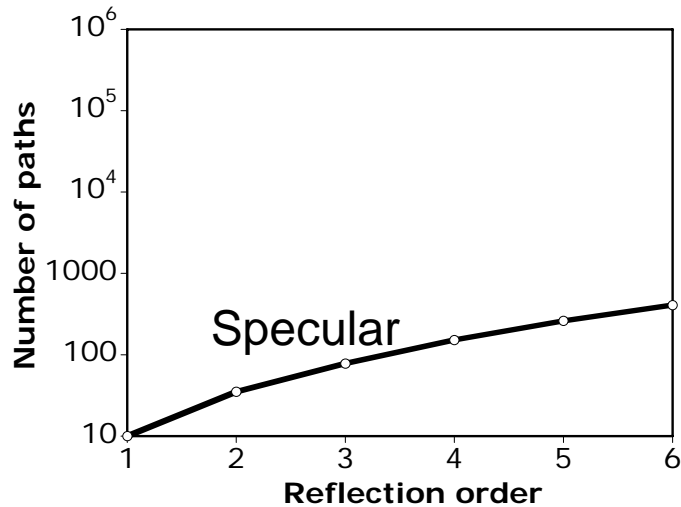
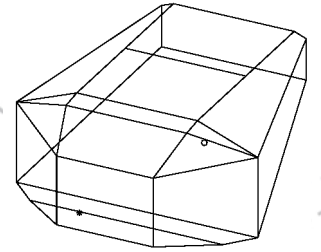
Exact edge diffraction solution exists only for diffraction from rigid wedge.

3. Zone-transitions (discontinuities)

Numerically robust techniques exist [Svensson and Calamia 2006]

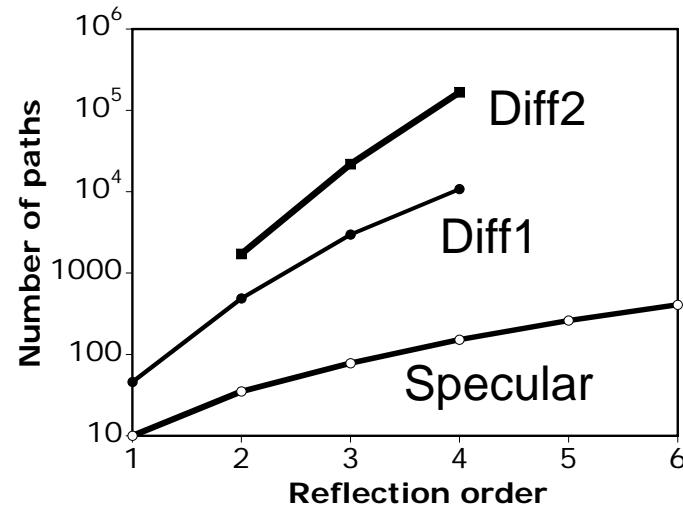
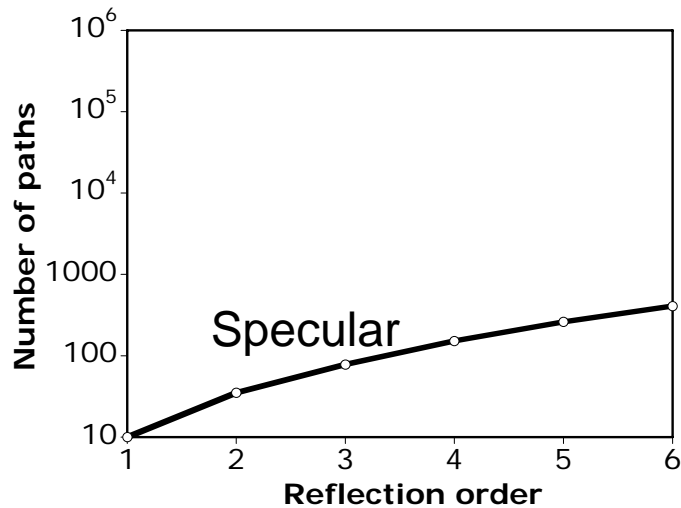
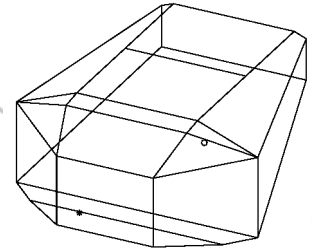
Challenge 1 - Rapid growth of number of components

Example from simple room: 19 planes, 36 edges
[Mechel, JSV 2002]



Challenge 1 - Rapid growth of number of components

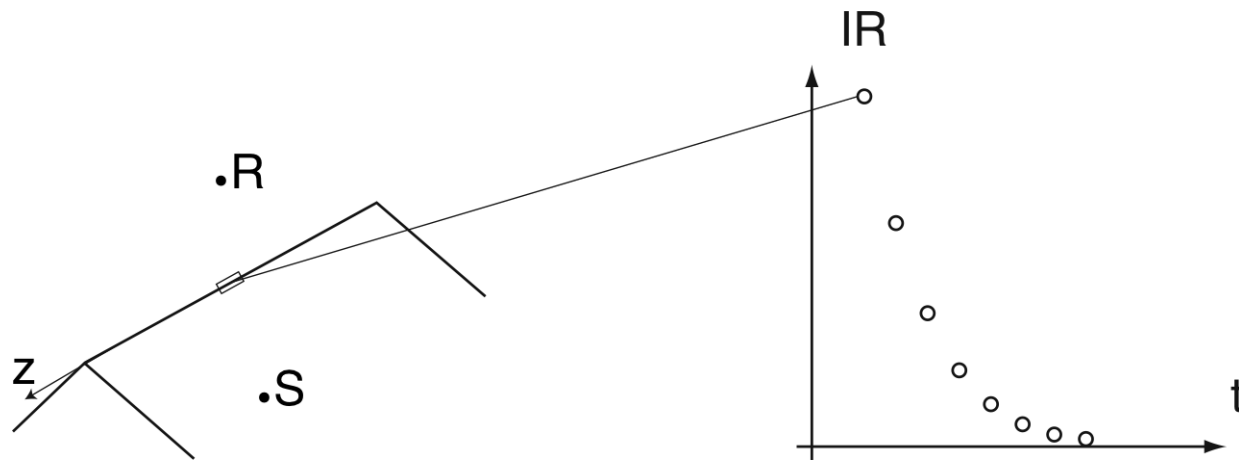
Example from simple room: 19 planes, 36 edges
[Mechel, JSV 2002]



Diff 1, refl order 3 = DSS,SDS,SSD

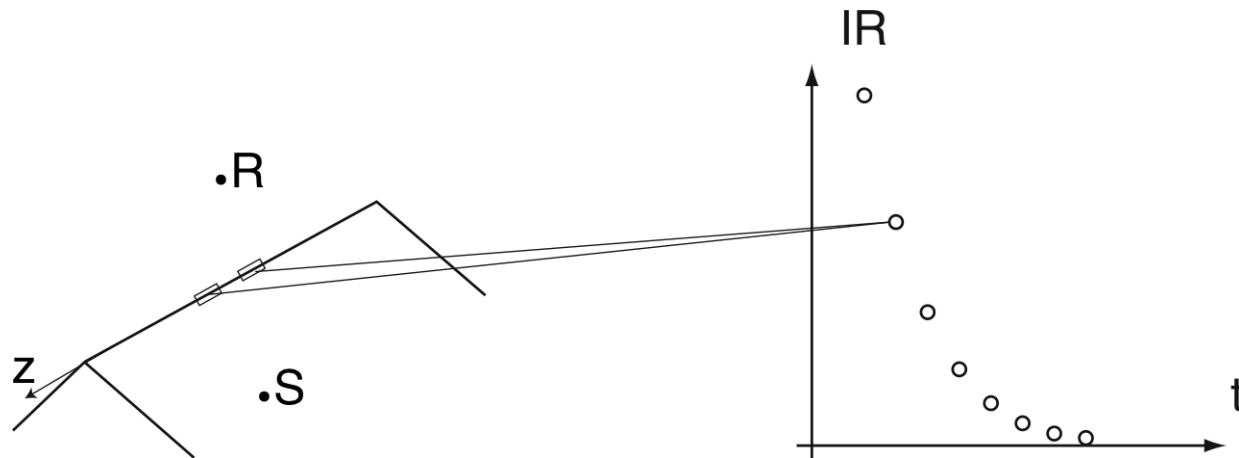
Computations involved in diffraction, 1

Each edge diffraction component IR requires a numerical integration for each sample value: a summing of contributions from points along the edge



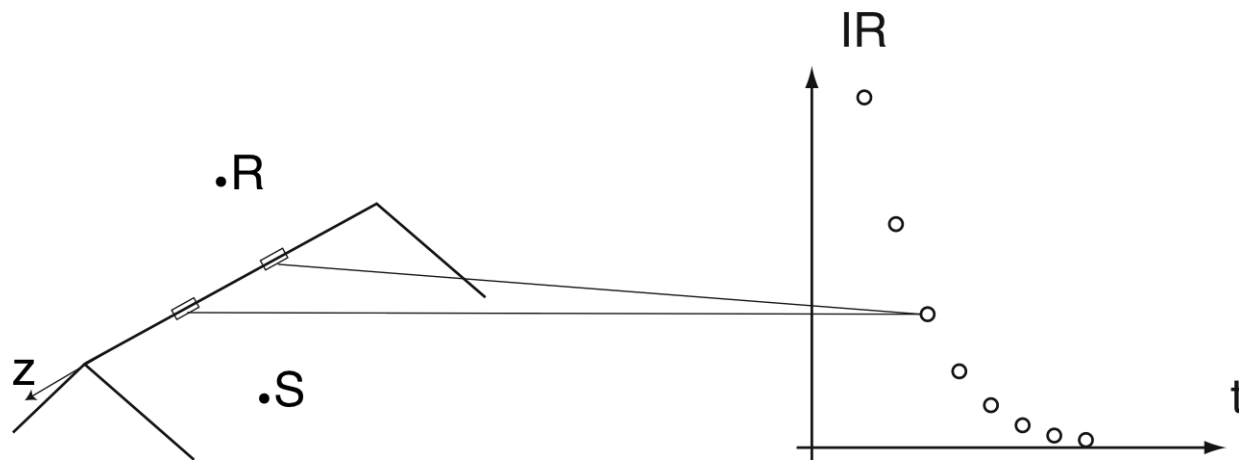
Computations involved in diffraction, 2

Each edge diffraction component IR requires a numerical integration for each sample value: a summing of contributions from points along the edge



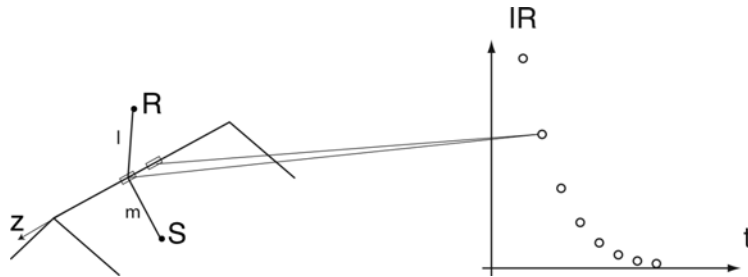
Computations involved in diffraction, 3

Each edge diffraction component IR requires a numerical integration for each sample value: a summing of contributions from points along the edge



Computations involved in diffraction, 4

The numerical integration for each sample value:



$$h_{diffr}(n) = -\frac{\nu}{4\pi} \sum_{i=1}^4 \int_{z_{n,1}}^{z_{n,2}} \frac{\beta_i}{ml} dz$$

$$\beta_i(z) = \frac{\sin(\nu\varphi_i)}{\cosh[\nu\eta(z)] - \cos(\nu\varphi_i)}$$

$$\eta(z) = \cosh^{-1} \left\{ \frac{ml + (z - z_S)(z - z_R)}{r_S r_R} \right\}$$

$$\varphi_1 = \pi + \theta_S + \theta_R$$

$$\varphi_2 = \pi + \theta_S - \theta_R$$

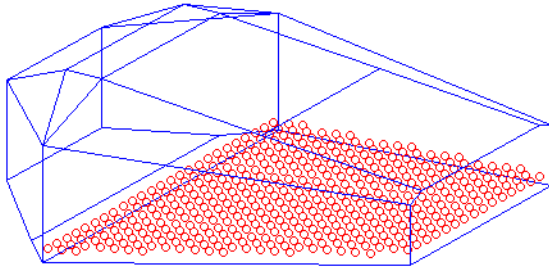
$$\varphi_3 = \pi - \theta_S + \theta_R$$

$$\varphi_4 = \pi - \theta_S - \theta_R$$

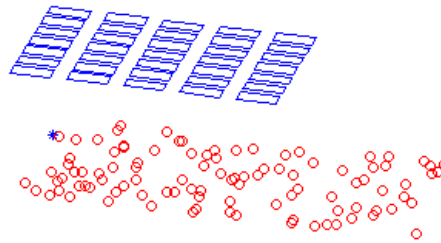
r_S, θ_S, z_S
 r_R, θ_R, z_R
 = cyl. coord.
 of S and R

Numerical examples

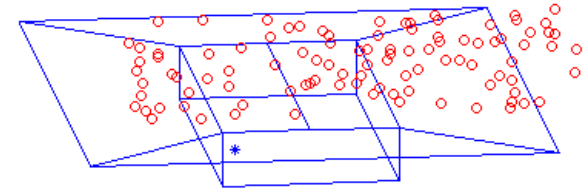
Hall



Reflector cloud



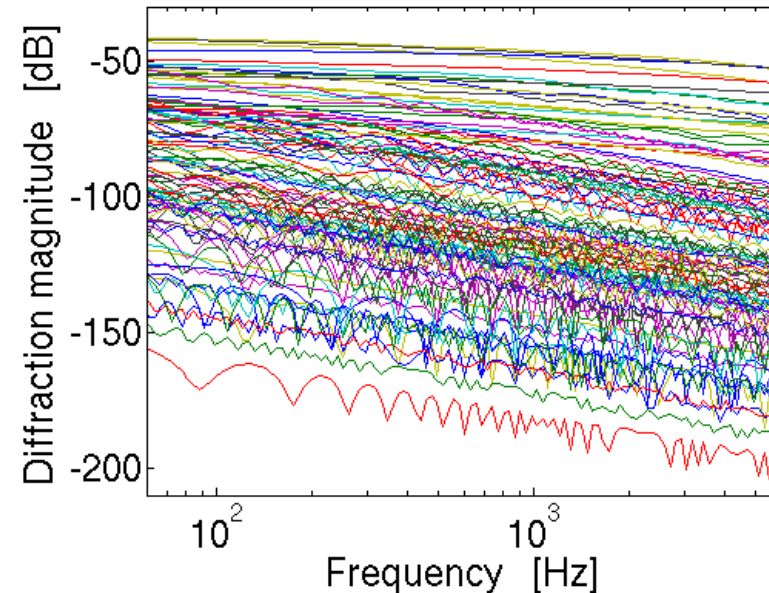
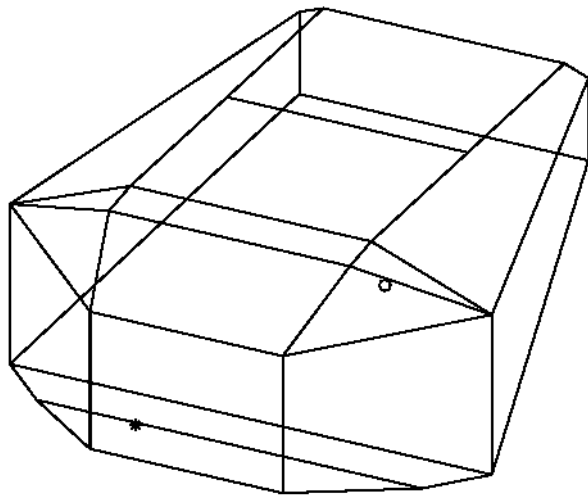
Orchestra pit



Chosen to represent a wide range. One source, many receiver positions. Hall from [Mechel 2002], Refl. cloud from [Calamia & Svensson 2006]. Orch. pit from [Løvstad & Svensson 2004].

Finding efficient pruning method

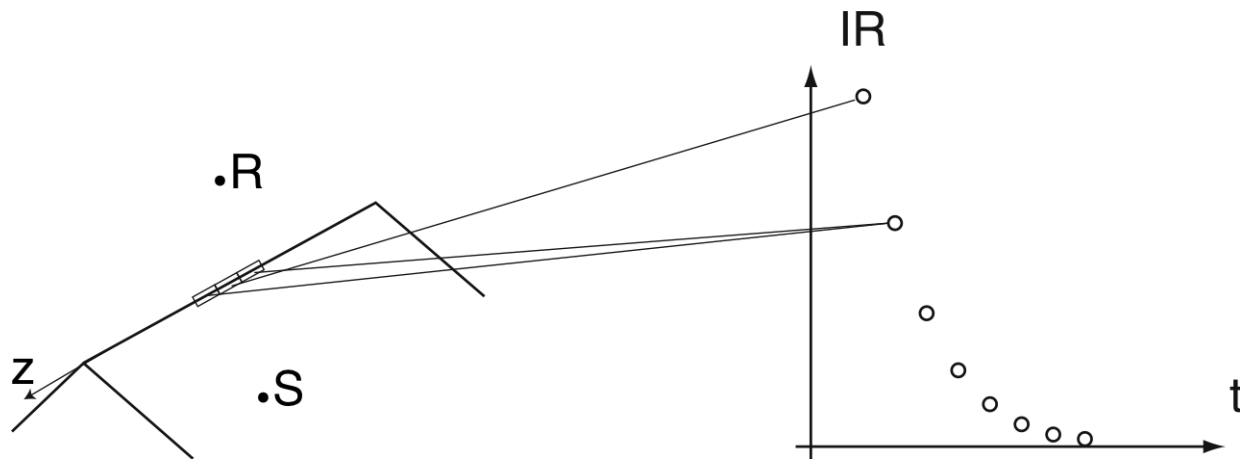
100 randomly selected diffraction IRs of type SDSS etc.



- Huge range of magnitude - possible to skip/prune some.
- Quite similar spectral shape - so we can look at average level as measure of importance.

Finding efficient pruning method

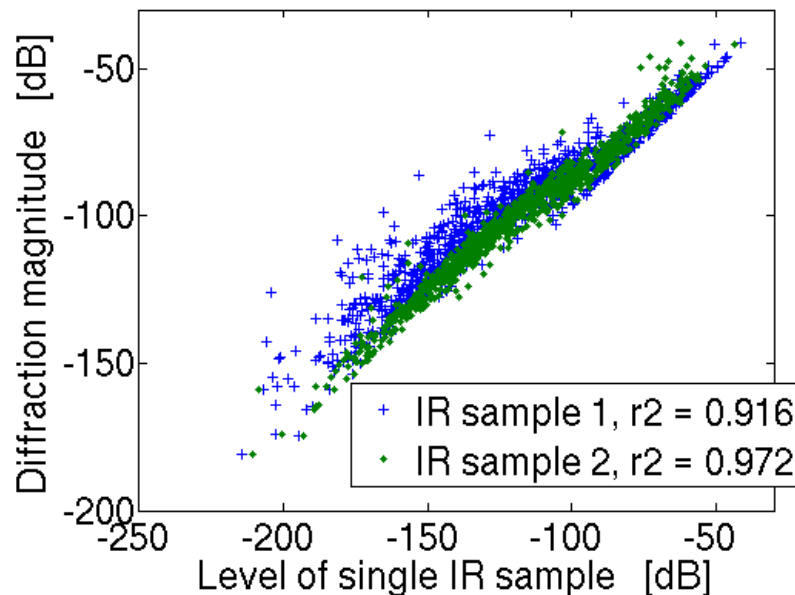
Candidate method - Compute first one or two sample values of diffraction IR (quick to compute)



Idea: since the IR almost always decreases monotonically, the start indicates how strong the rest would be.

Finding efficient pruning method

Candidate method - Compute first one or two sample values of diffraction IR (quick to compute)



High correlation between value of IR sample 1 or 2 and total diffraction IR energy
⇒ useful pruning criterion.

Suggested pruning method

For each of N diffraction components (N is large):

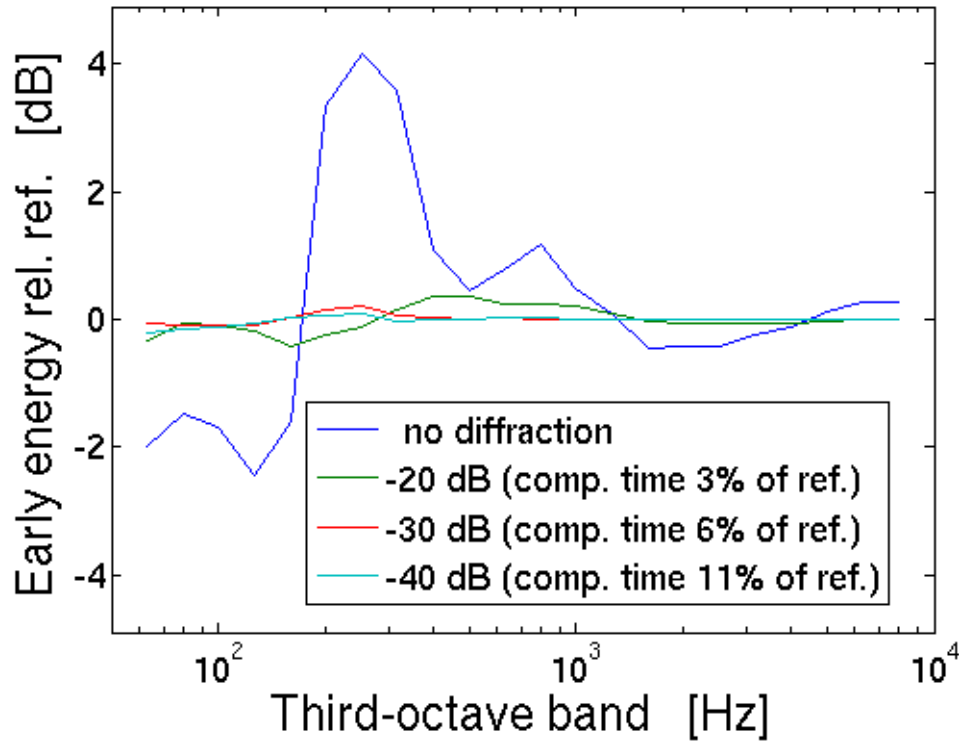
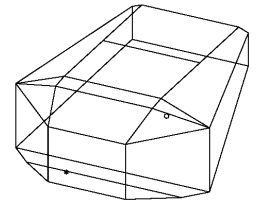
Compute IR sample values 1 and 2 (quite fast)

If IR sample value 2 $>$ limit value, then

Compute full IR (time-consuming)

Limit value can be based on global maximum, or the maximum found so-far.

Evaluation of pruning method - Hall



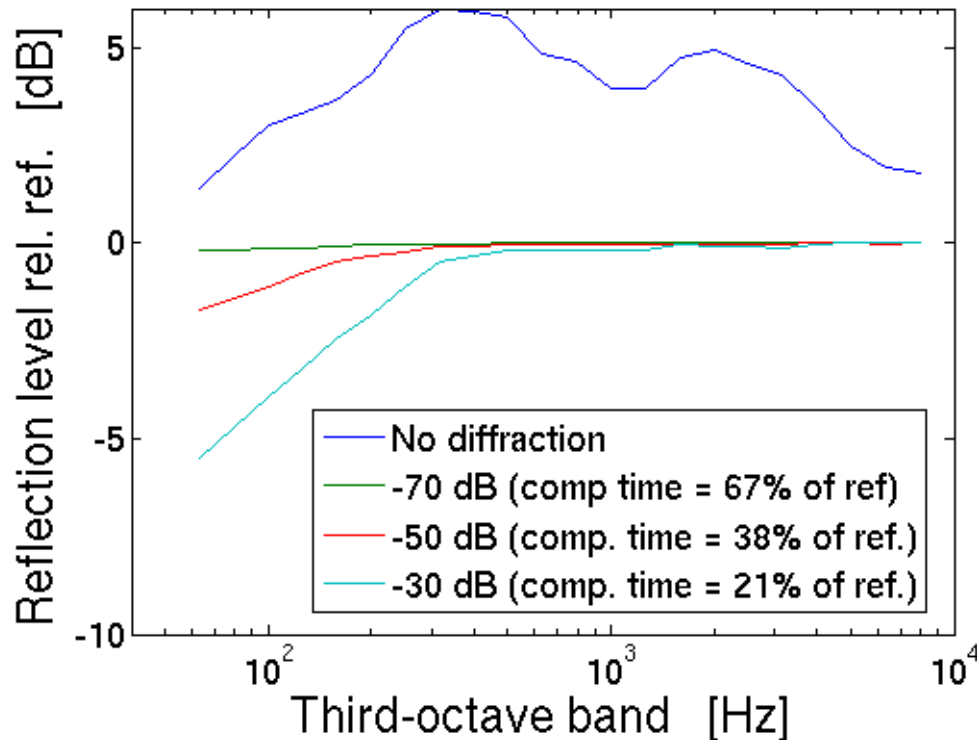
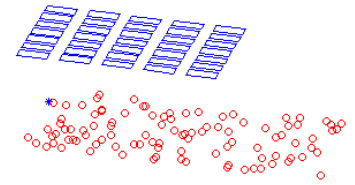
Single rec. pos.
 Single diff. + up to 3rd order spec. ⇒ 10634 diffraction components.

Many components can be pruned in interior geometry.

Diffraction important mainly at LF.

Ref = include all diffraction components

Evaluation of pruning method - Reflector cloud

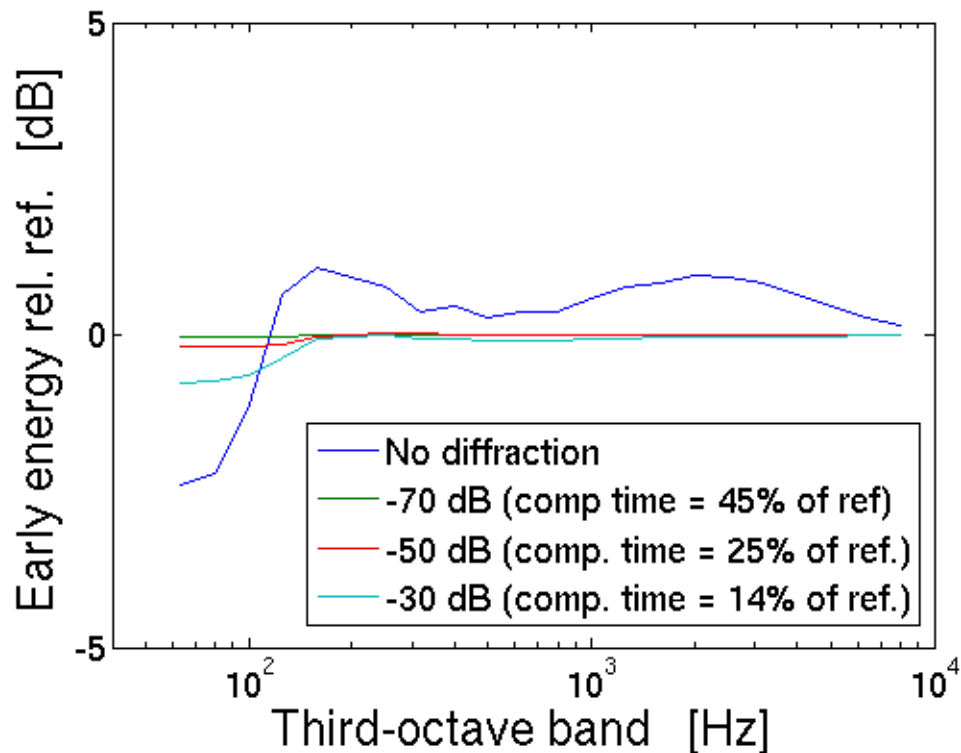
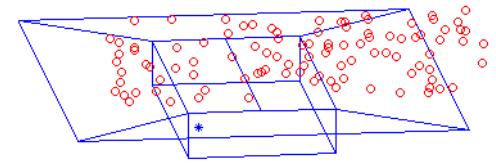


Average results for 100 rec. positions.

Diffraction much more critical than in hall, also at higher frequencies.

NB! Without diffraction, 48 out of 100 rec. pos. get zero reflection!

Evaluation of pruning method - Orchestra pit



Average results for 100
rec. positions. Up to 6th-
order combinations.

Diffraction not so critical
for the early energy.

Pruning quite efficient.

Conclusions

The huge number of diffraction components can be alleviated by first computing the first one or two samples of each diffraction IR. Based on their values, a decision is made on whether the rest of the IR is worth computing or not.

Some edges need more stringent criteria, typically reflector edges. They contribute at low and high frequencies.

Interior edges contribute significantly only at lower frequencies - but should not be ignored.

References

- M. A. Biot, I. Tolstoy, "Formulation of wave propagation in infinite media by normal coordinates with an application to diffraction," *J. Acoust. Soc. Am.* 29, pp. 381-391 [March 1957].
- P. T. Calamia, U. P. Svensson, "Edge subdivision for fast diffraction calculations," in *Proc. of 2005 IEEE Workshop on Applications of Signal Processing to Audio and Acoustics (WASPAA)*, New Paltz, NY, pp. 187-190 [2005].
- A. Løvstad, U. P. Svensson, "Scale model measurements of an orchestra pit," *Acoust. Sci. Tech.* 26, pp. 237-239 [2005].
- F. P. Mechel, "Improved mirror source method in room acoustics," *J. Sound Vib.* 256, pp. 873-940 [2002].
- Herman Medwin, Emily Childs, Gary M. Jepsen, "Impulse studies of double diffraction: A discrete Huygens interpretation," *J. Acoust. Soc. Am.* 72, pp. 1005-1013 [Sept. 1982].
- H. Medwin, "Shadowing by finite noise barriers," *J. Acoust. Soc. Am.* 69, pp. 1060-64 [April 1981].
- U. P. Svensson, P. T. Calamia, "Edge-diffraction impulse responses near specular- and shadow-zone boundaries," *Acta Acustica/Acustica* 92, pp. 501-512 [2006].
- U. P. Svensson, R. I. Fred, J. Vanderkooy, "An analytic secondary source model of edge diffraction impulse responses," *J. Acoust. Soc. Am.* 106, pp. 2331-2344 [1999].
- P. Svensson, K. Wendlandt, "The influence of a loudspeaker cabinet's shape on the radiated power," in *Proc. of Baltic Acoustic 2000*, Vilnius, Lithuania, Sept. 17-21; *J. of Vibroeng.*, No. 3(4), pp. 189-192 [2000].