



# Low Frequency Limits of Reflector Arrays

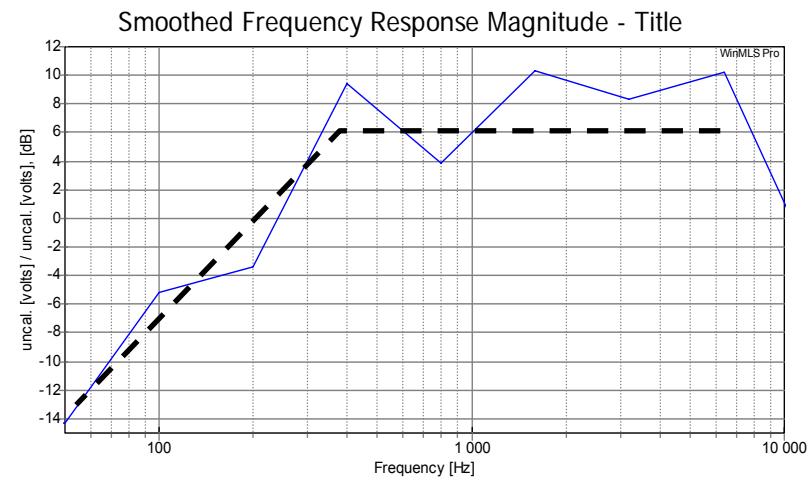
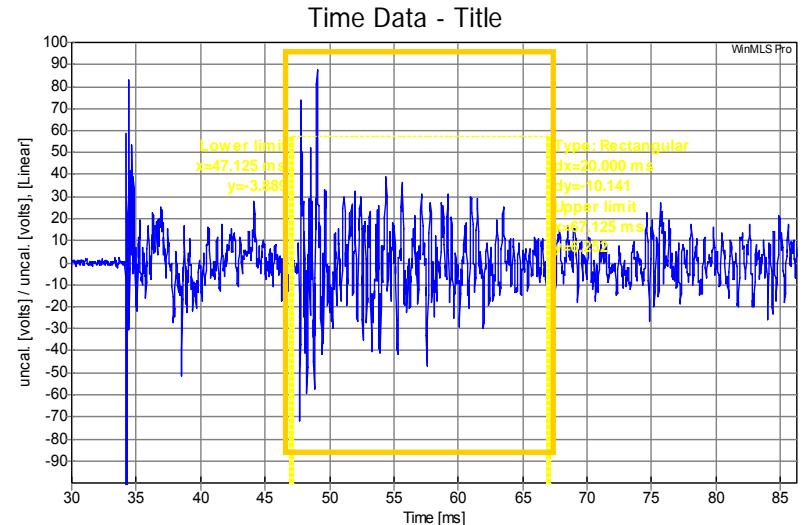
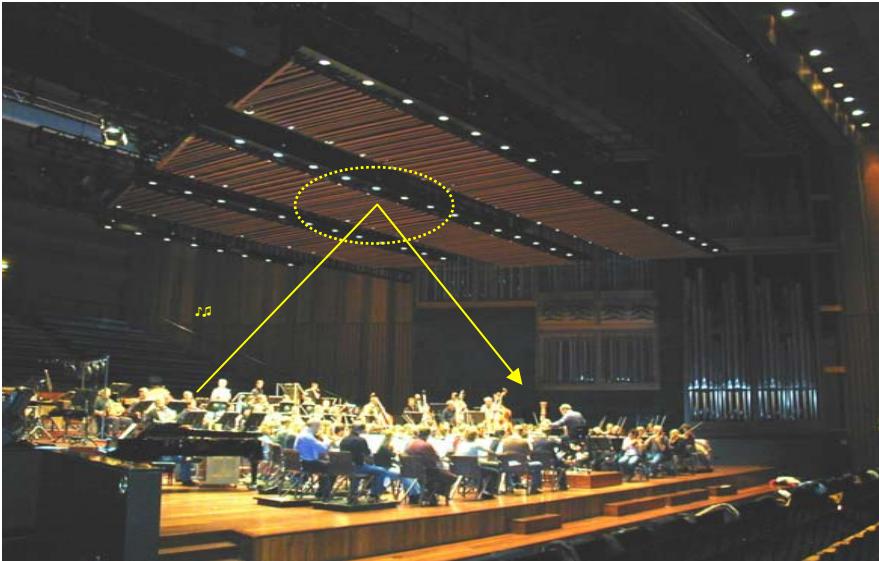
Measurements and theory on flat, thin panels

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[www.akutek.info](http://www.akutek.info)

# Background: Orchestra Canopy



- Reflection
- Time window
- Freq. response

# Reflector array prediction

- Fresnel-Kirchhoff (FK), Rindel (1991):

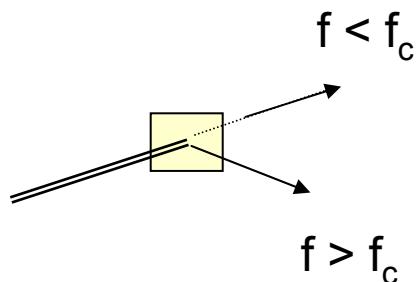
$$L = 20 * \log(\mu)$$

$\mu$  = panel area / array area

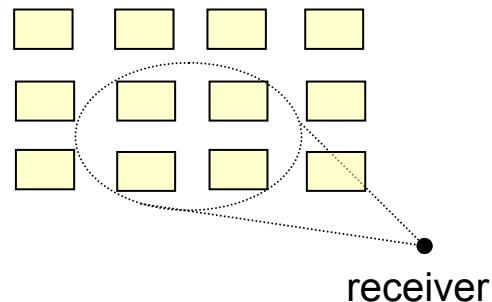
- FK assumes “perfect” reflectors
  - Sufficiently rigid
  - Large compared to wavelength: Leonard, Delsasso, Knudsen (1964)
- Reflectors are NOT perfect for **larger  $\lambda$**

# Two filters

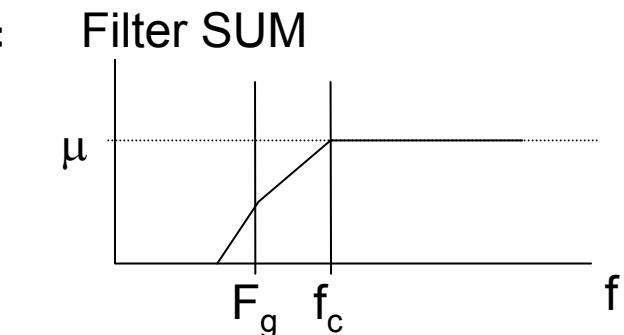
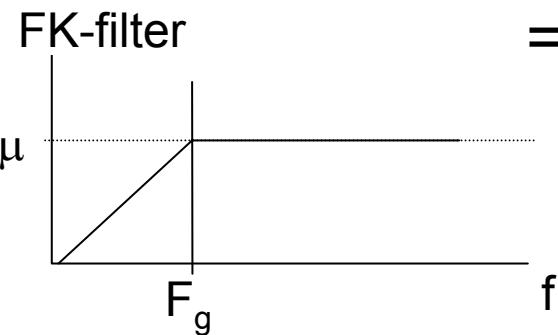
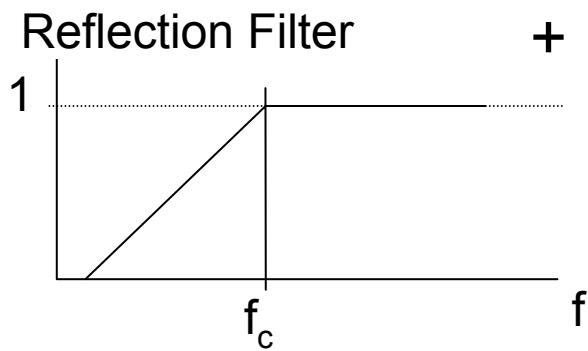
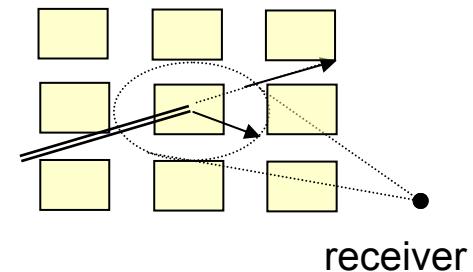
Ability to reflect sound



Sensitivity towards reflector



Received reflection



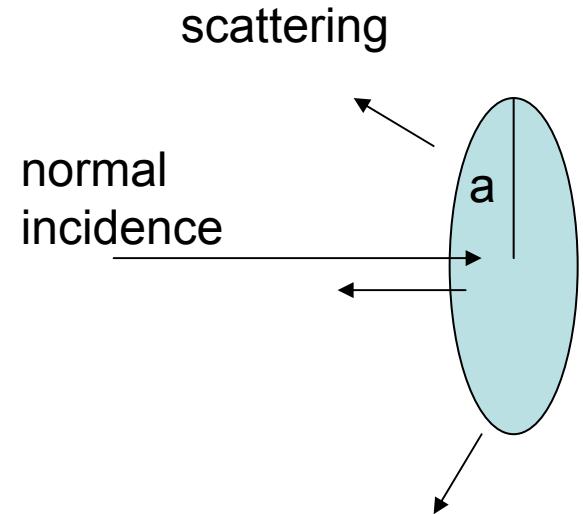
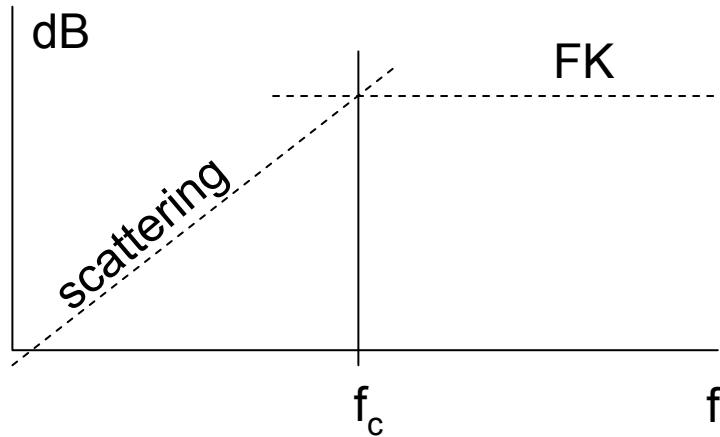
$F_g$  by Rindel (1991)

$f_c = ?$

# Example: Disc $f_c$

- $f < f_c$  asymptote: Scattering from disc, normal incidence (Pierce 1981)
- $f > f_c$  asymptote: Fresnel-Kirchhoff (FK)

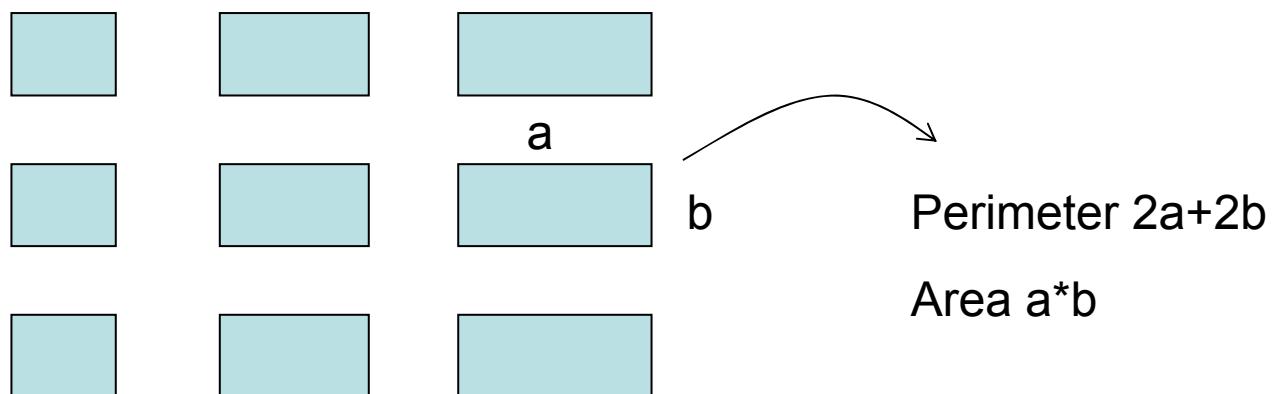
$$f_c \approx 64 \cdot \frac{\text{perimeter}}{\text{area}}$$



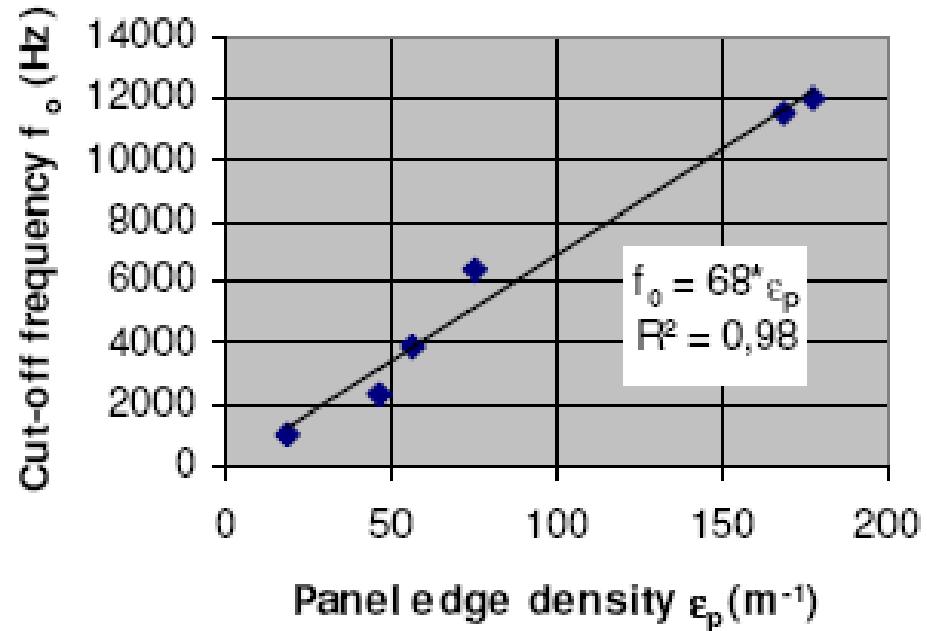
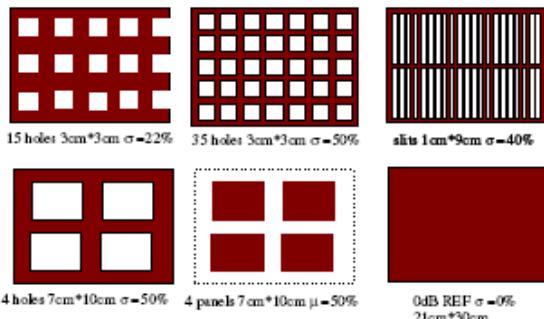
# Hypothesis

$$f_c \approx C \cdot \frac{\sum \text{perimeter}}{\sum \text{area}} = C \cdot \varepsilon$$

$f_c$  critical frequency of array Reflection Filter  
 $\varepsilon$  Panel Edge Density of array  
 $C$  constant to be determined



# Scale model test



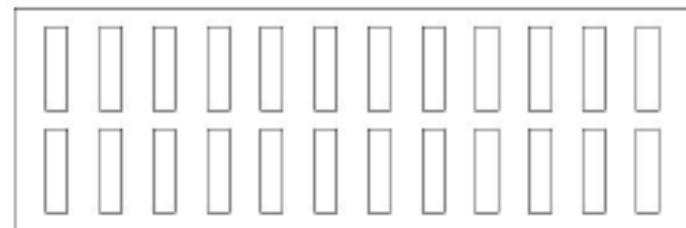
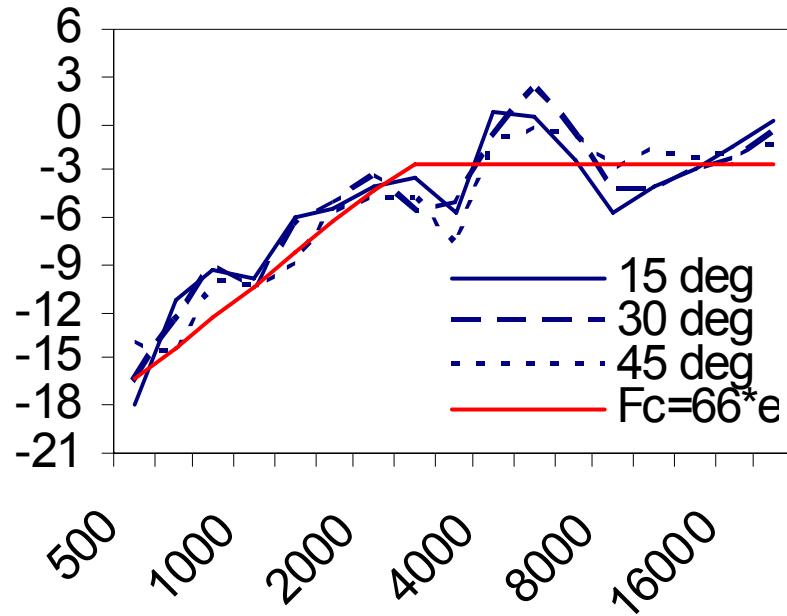
- Scale model test trend:  $f_c = 68 * \epsilon$
- $R^2 = 0.98$
- Theory on discs:  $f_c = 64 * \epsilon$

# More tests

- Different shapes (normal incidence)
- 40 model arrays with different element shapes and patterns (Student project, NTNU, Trondheim):
  - Trend:  $f_c = 67^* \varepsilon \pm 11\%$  (disc theory  $64^* \varepsilon$ )
  - Comment: Uneven frequency responses due to FK-effects leaves some uncertainty.

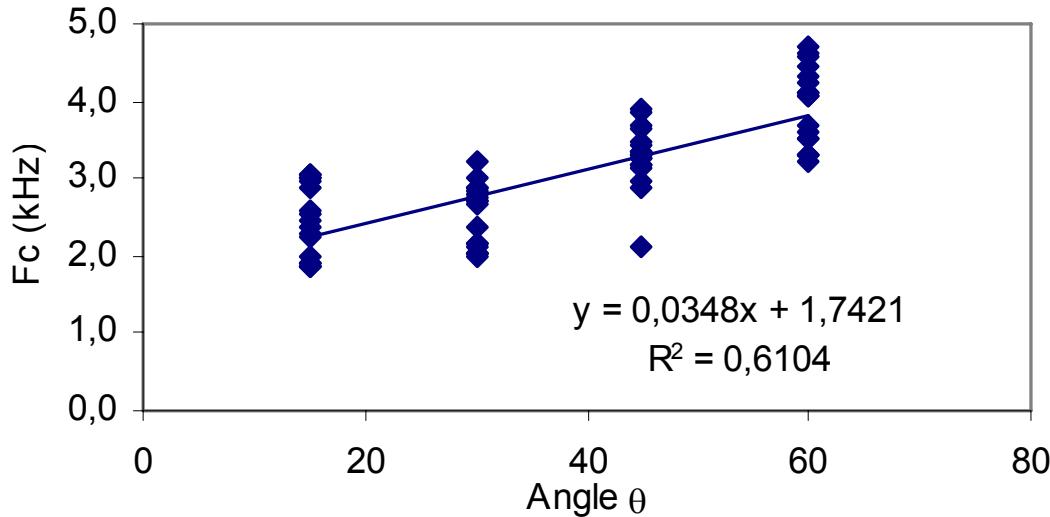
# Incidence angle

- Reflection filter “drowning” in FK-effects:
- Interference
  - Due to periodic array geometry
- Dips and peaks move with angle
- FR's sensitive to position



Scale model measurements by Thorød, NTNU, Trondheim 2006

# Incidence angle



- $f_c$  correlates ( $R^2$ ) only 61% with angle
- $f_c$  variation can be explained by FK alone
- Hypothesis “**Reflection Filter is angle-independent**” may still hold

# Further work

- $f_c$  -predictor must be confirmed
  - More tests on different panel shapes
  - More tests on oblique incidence
  - More theoretical tests
- Search for array geometries with frequency responses close to ideal high-pass filter
  - To provide good reflected sound quality
  - To make  $f_c$ -detection easier

# Canopy design issues

- $f > 400\text{Hz}$  fill-in important, since through-the-orchestra path is obstructed
  - > elements must be large enough
- Smooth FR's up to 4kHz important
  - > elements must not be too large
- Higher position – wider frequency range
  - but later and weaker response
- Lower position – array should be less dense
  - to prevent stage separated from auditorium

# Conclusions

$$\mathbf{f}_c = C^* \boldsymbol{\varepsilon}$$

at normal incidence for some geometries

- $C$  apparently in the interval  $\sim 64\text{-}68$
- Must be tested for generality: Different array geometries and incidence angles
- Smooth FR's should be pursued
- 400-4000Hz important for canopies
- Canopy arrays inherently narrow-banded
- Optimum panel size and shape important



# Thank you!

- Full paper:  
[http://www.akutek.info/Papers/MS\\_Array\\_2007.pdf](http://www.akutek.info/Papers/MS_Array_2007.pdf)
- Acoustics, research, papers, more:  
[www.akutek.info](http://www.akutek.info)
- ICA 2007 homepage:  
<http://www.ica2007madrid.org/>